

A Look at how Workpiece Position Affects Manufacturing Tolerances

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Abstract

The purpose of manufacturing tolerancing is to determine the part's intermediate geometrical and dimensional states during the production process. These production dimensions also serve to meet manufacturing restrictions, such as machine geometrical errors, vibration, and cutting tool wear, in addition to the functional requirements specified in the definition drawing.

The placement decision has a significant impact on manufacturing costs and quality. A two-step technique has been created to circumvent this difficulty. The initial stage is determining the best possible posture. In the second stage, researchers looked at the effect of tightening the tolerance interval.

Keywords: Dispersion, tolerance, manufacturing, position.

INTRODUCTION

Precision plays a crucial part in the modern company's rivalry. In the sphere of manufacturing, it is difficult to realise items in unit or series with the same accuracy, i.e. with the same dimensions. This inexorable inaccuracy is caused by a

variety of variables, including positioning errors, vibrations, tool wear during milling, and stop placement. These characteristics are referred to as dispersions of machinings in the technical literature, and they are divided into two

types: random dispersion and systematic dispersion.

Many research studies have addressed the tolerancing problem in various ways; presented the AUTOFIX system, which allows the manufacturing assembly to be conceived based on the geometry of the component and the phase organisation. Perremans has created the IDEFIX computer, which allows users to design all of the fixings needed to construct a prismatic item.

Rong and Bai investigated a dependent connection of operational dimensions in order to quantify machining mistakes in terms of workpiece linear and angular dimensions. Cai et al. suggested a technique for performing a robust fixture design in order to reduce workpiece positional mistakes caused by workpiece surface and fixture setup faults. Djurdjanovic and Ni devised techniques for calculating the impact of fixture errors, finding datum features, and measuring datum features on machining dimensional errors. These analyses were carried out under the assumption of a static situation. Hirsch introduced the MCOES method for designing a machine assembly that ensures participation in the assembly of pieces from the same family.

The user creates a mechanism for mounting a spare for each household interactively. A research on the impact of the cutting tool's location on the dynamic behaviour in thin wall milling was published, and the authors depict the influence of the cutting tool's route on the surface.

The purpose of research is to look at the impact of systematic dispersion on production tolerances. Sebaa presented a mathematical methodology for calculating the Fulcrum distribution.

Our research focuses on the impact of placement dispersion on production tolerances.

EXPERIMENTAL STUDY

The goal of this component is to investigate the impact of positioning inaccuracy on production tolerances. Two steps are devised to do this.

A. First Step

The goal of this stage is to find the isostatic position that is best for you. We ran a 100-trial test to attain this aim, as shown in Fig. 1. Figure 2 is a measuring example.

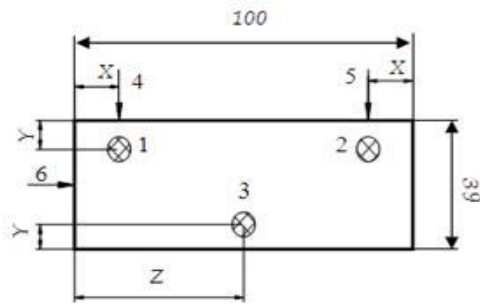


Fig. 1 Fulcrums variation



Fig. 2 Example of measurement

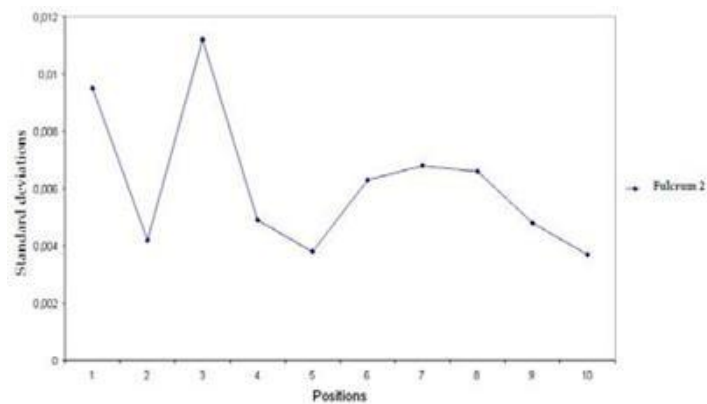


Fig. 3 Standard deviations of the Fulcrum 1 according to the number of trials

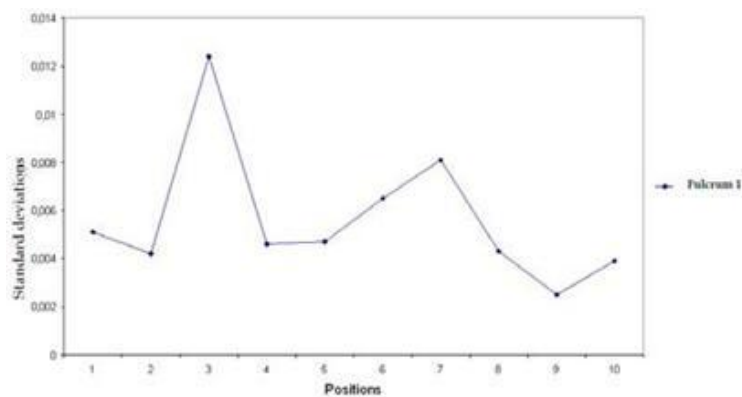


Fig. 4 Standard deviations of the Fulcrum 2 according to the number of trials

Figure 3 demonstrates how the standard deviations of the Fulcrum 1 have changed over time as the number of trials has increased. The chosen places range from 0.002 to 0.014. The best position for Fulcrum 1 is thus position 9.

Figure 4 demonstrates how the standard deviations of the Fulcrum 2 have changed over time as the number of trials has increased. The chosen places range from 0.003 to 0.012. The best position for Fulcrum 2 is thus position 10.

Figure 5 demonstrates how the standard deviations of the Fulcrum 3 have changed over time as the number of trials has increased. The chosen places range from 0.0025 to 0.012. The best location for Fulcrum 3 is thus position 6.

Figure 6 demonstrates how the standard deviations of the Fulcrum 4 have changed over time as the number of trials has

increased. The chosen places range from 0.002 to 0.035. The best position for Fulcrum 4 is thus position 10.

Figure 7 demonstrates how the standard deviations of the Fulcrum 5 have changed over time as the number of trials has increased. The chosen places range from 0.002 to 0.035. The best location for Fulcrum 5 is thus position 10.

Figure 8 demonstrates how the standard deviations of the Fulcrum 5 have changed over time as the number of trials has increased. The chosen places range from 0 to 0.035. Positions 3, 8, and 10 therefore provide the ideal position.

We extract the distribution of Fulcrum optimum from it according to the graphs in Figs. 3-8 in order to find the smallest mistake. The ideal distribution is seen in Figure 9.

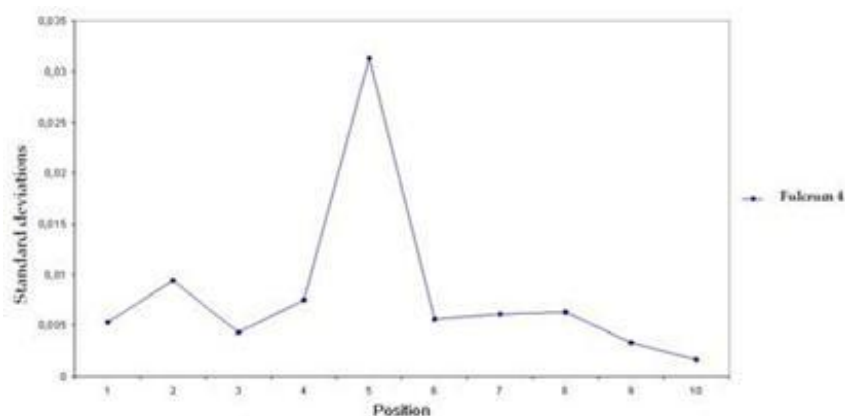


Fig. 5 Standard deviations of the Fulcrum 3 according to the number of trials

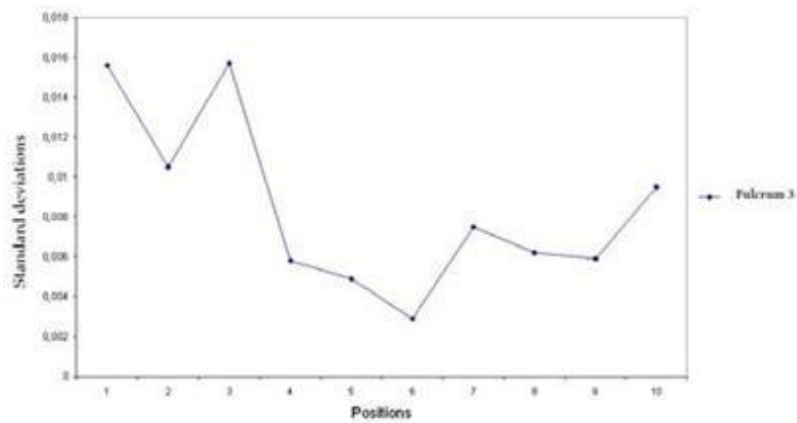


Fig. 6 Standard deviations of the Fulcrum 4 according to the number of trials

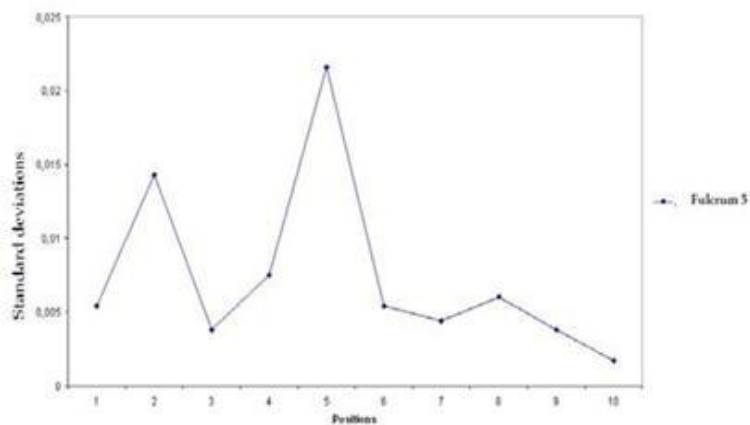


Fig. 7 Standard deviations of the Fulcrum 5 according to the number of trials

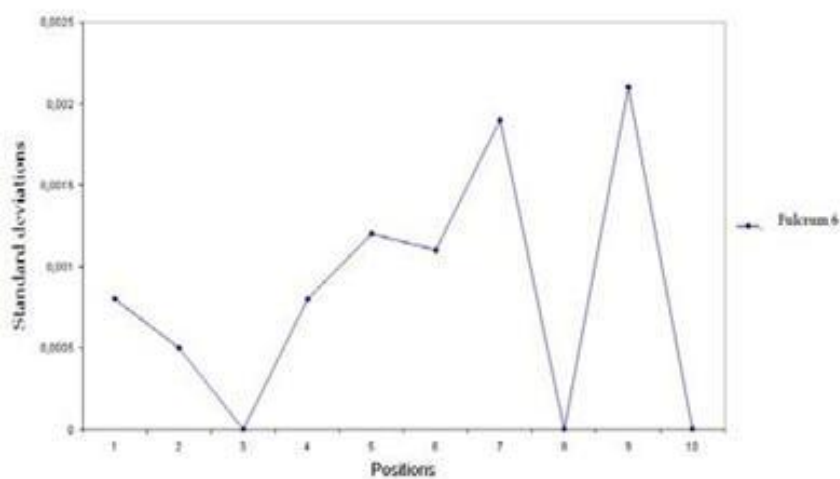


Fig. 8 Standard deviations of the Fulcrum 6 according to the number of trials

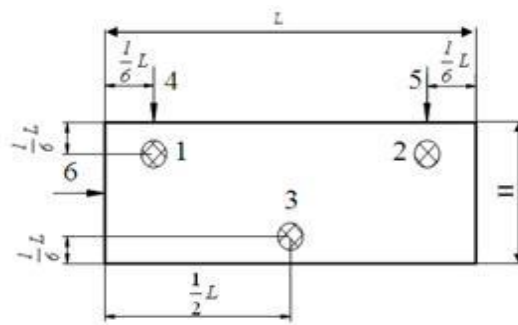


Fig. 9 Optimal position

B. Second Step

We measure the flaws of placing in position under the impact of tightening and determine the standard deviations of each Fulcrum at this ten-try stage. We use the ideal position to measure the flaws for each tightening.

Figure 10 depicts an example of defect measurement with tightening.



Fig. 10 Example of measurement

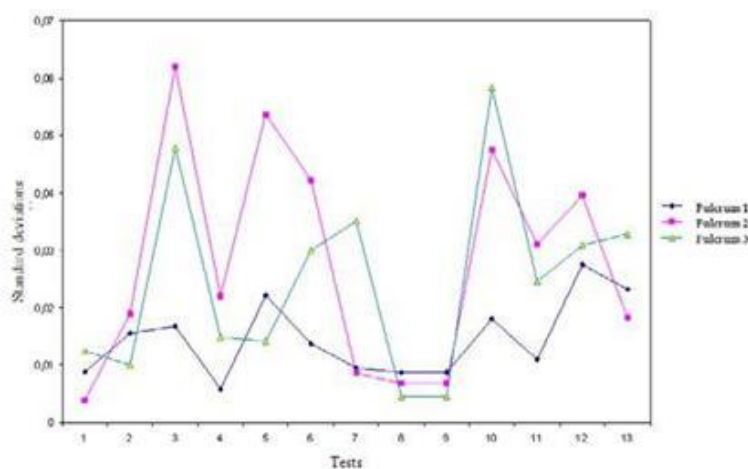


Fig. 11 Standard deviations of the Fulcrum plan under the influence of tightening according to the trial number

According to the trial number, Fig. 11 depicts the growth of the standard deviation of the Fulcrums plan specified by the Fulcrums 1, 2, and 3.

We can see from the graphs (Fig. 11) that Fulcrum 2 and Fulcrum 3 have significant inaccuracies in the majority of the places.

Figure 12 shows how the standard deviation of the linear Fulcrum formed by

Fulcrums 4 and 5 changes as the trial number increases. Due to the phenomena of both Fulcrums 4 and 5 tightening, we note that both graphs are parallel.

The standard deviation of the punctual Fulcrum (6) is shown in Fig. 13 as a function of the trial number. We can see that the graph of the Fulcrum 6 is always nil; this is owing to the Fulcrum's punctual contact.

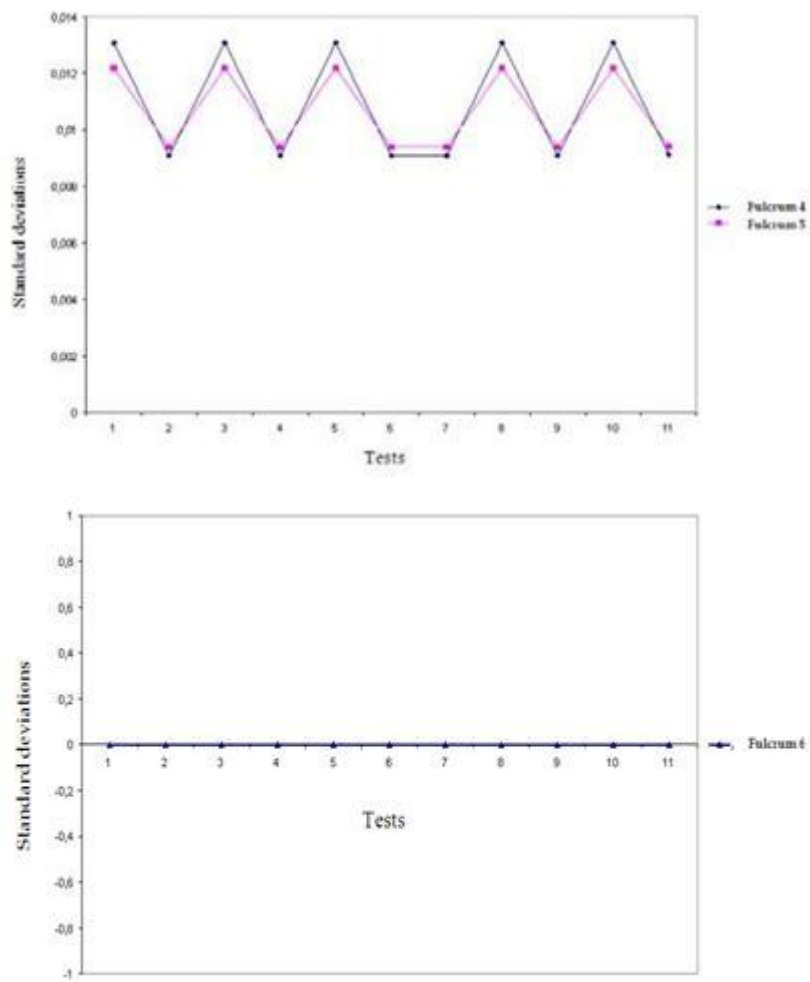


Fig. 13 Standard deviations of the punctual fulcrum under the influence of tightening

CONCLUSION

We offered two phases in this study for calculating the dispersion of the placing in place and influencing the manufacturing tolerances. It follows that the ideal distribution of the Fulcrums is as follows: 1/6 for the Fulcrums 1, 2, 3, 4, and 5, 1/2 for the Fulcrum 6. Even with the best allocation, we discovered that the tightening effect had a significant impact on part quality.

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